

Hot forming and characterization of forming behavior of three Fe-Mn-C high-manganese steels

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- **Motivation**
- **Material Characterization**
 - **Processing of compression tests**
 - **Results of compression tests**
- **Material Production**



Motivation

Field of research: Hot and cold forming of ternary Fe-Mn-C HMS

Goals: Production of hot and cold rolled HMS sheets in laboratory scale and numerical simulation of the forming process

Comparison of the forming behavior to industrially applied austenitic steel

Needed: Flow curves in dependence of strain, strain rate, temperature and chemical composition

→ → → Investigation of the influence of

- Carbon content
- Manganese content
- Strain rate
- Temperature

Method: Characterization of three ternary Fe-Mn-C steels and reference austenitic chromium nickel steel 1.4301 / AISI 304 by compression tests



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Material characterization – material description

Material within the SFB 761

- 8 compositions of Fe-Mn-C steels are planned
- Cast in a vacuum induction facility at Institute of Ferrous Metallurgy, RWTH Aachen
- Batches weighting approx. 70-100 kg
- Here 3 compositions are investigated:
 - I: Mn22C0.3 “TRIP”
 - II: Mn22C0.6 “TWIP”
 - III: Mn28C0.3 “TWIP”

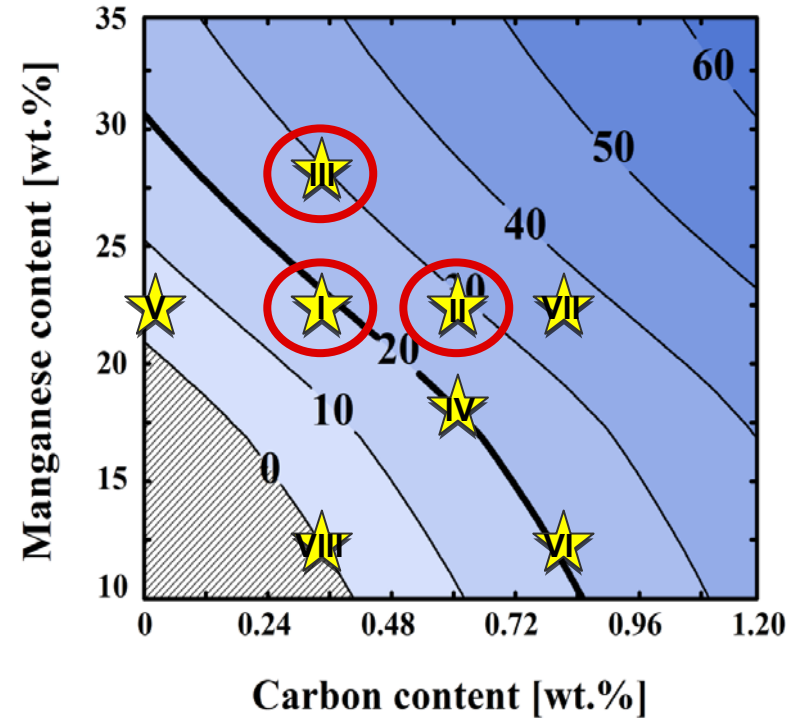


Diagram of steel compositions within SFB 761

SFE calculated by Saeed-Akbari, Institute of Ferrous Metallurgy, RWTH Aachen¹

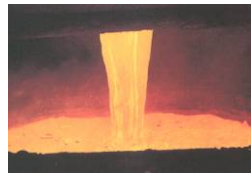
OES analysis of tested materials (cast state)

OES performed at Institute of metallurgy and metal recycling, RWTH Aachen

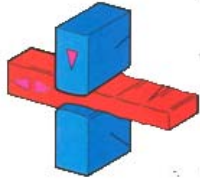
name / cont. wt. %	Fe	C	Mn	Si	P	S	Cr	Ni	Mo	Al	Cu	Co	Nb	V	N
Mn22C0.3, I (V16)	Bal.	0.34	22.65	0.14	0.01	0.00	0.30	0.01	0.05	0.01	0.01	0.01	0.02	0.01	0.01
Mn22C0.6, II (V15)	Bal.	0.57	23.21	0.17	0.01	0.00	0.31	0.02	0.04	0.01	0.01	0.01	0.01	0.01	0.01
Mn28C0.3 III (V19)	Bal.	0.28	28.12	0.10	0.01	0.00	0.02	0.04	0.02	0.01	0.01	0.01	0.02	0.02	0.02

¹) Saeed-Akbari, A.; Imlau, J.; Prah, U. and Bleck, W., Derivation and Variation in Composition-Dependent Stacking Fault Energy Maps Based on Subregular Solution Model in High-Manganese Steels, Metallurgical Materials Transactions A, Vol. 40A, Dec. 2009, pp. 3076-3090

Material characterization – processing of compression tests



Casting



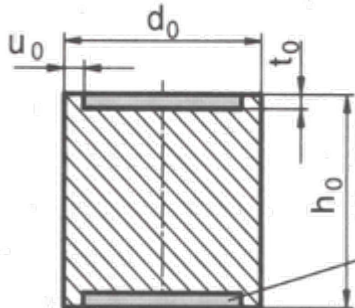
Forging



Annealing



Rastegaev-geometry



Lubrication:

- Up to 300°C: Teflon
- Up to 700°C: Graphite
- 700 - 800°C: Boron-nitride
- 800 - 1.300°C: Glass



before test after test

Input: Cast blocks (140*140 mm² cross section)

Forging of cast blocks in 4 steps to 20 mm height (initial temperature 1150°) and annealing (1150°C / 5h)

Processing: Isothermal compression tests

- Rastegaev cylinders (15 mm height, 10 mm diameter, lubrication slots)
- Temperatures (RT and 300 to 1200°C)
- Constant strain rates (0.1, 1 and 10 1/s)
- Computer controlled 1200 kN servohydraulic testing system, SERVOTEST LTD.

Calculation of stress (kf) and strain
(temperature compensation (300 to 1200°C))

B. Wietbrock, W. Xiong, M. Bambach, W. Xiong, G. Hirt: Steel research international, 82 (2011) No. 2, pp. 127-136.
W. Xiong, B. Wietbrock, A. Saeed-Akbari, M. Bambach, G. Hirt: Steel research international, 82 (2011) No. 1, pp. 63-69

Material characterization – temperature compensation

Assumptions and calculation

- Upsetting test in enclosed oven is adiabatic
- Totally in the specimen brought energy density corresponds to the surface below the flow curve
- Results in rise of temperature:

$$\Delta T_{total} = \frac{\int \sigma d\phi}{\rho \cdot C_p} \cdot D$$

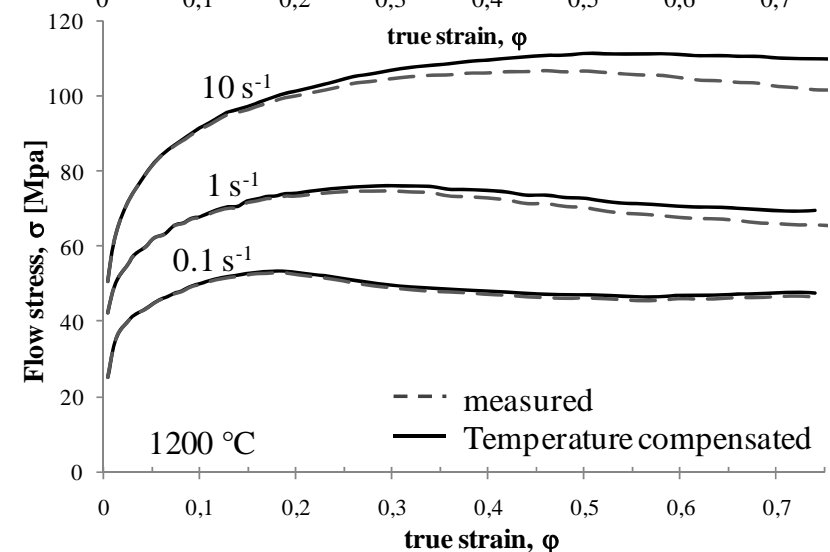
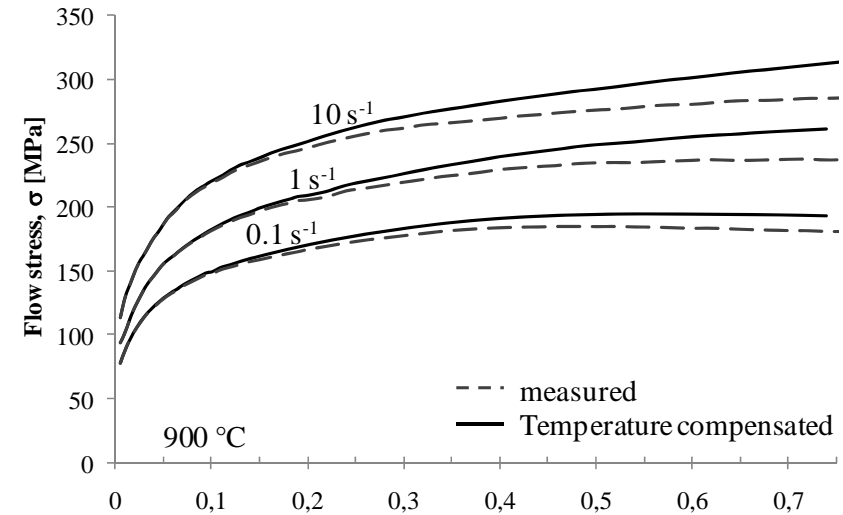
- Temperature dependent ρ and C_p^* , $D=0.9$

$$\Delta T_{HT} = \frac{2 \cdot \alpha}{\rho \cdot C_p \cdot h} \cdot (T_{t-1} - T_{die}) \cdot \Delta t$$

- α T-dependent (α by inverse modelling)
- Calculation of temperature of flow state

$$\Delta T = \Delta T_{total} - \Delta T_{HT}$$

- Flow curve (T-compensated) calculation by regression and interpolation



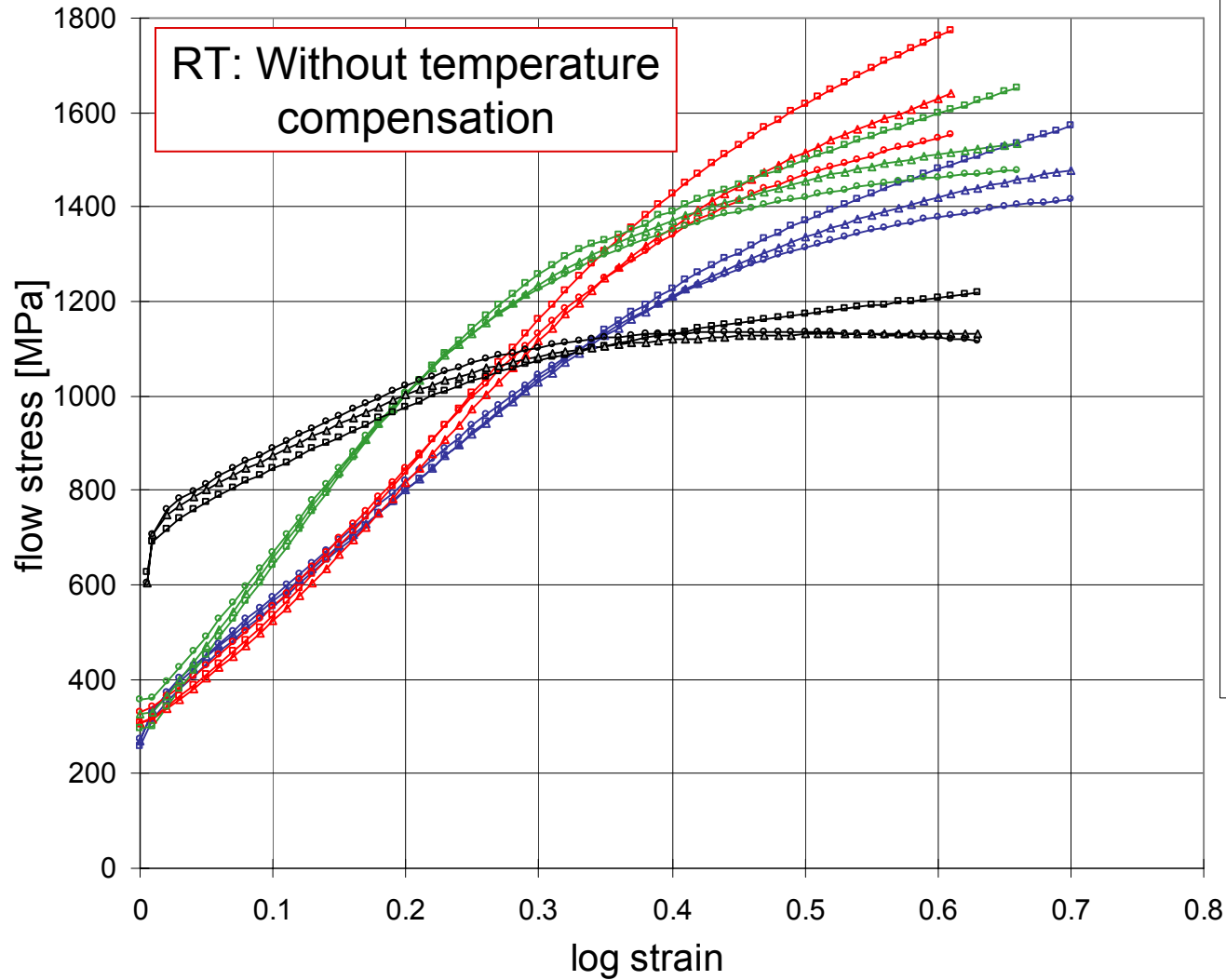
Examples for T-compensation of Fe-Mn22-C0.6

B. Wietbrock, W. Xiong, M. Bambach, W. Xiong, G. Hirt: Steel research international, 82 (2011) No. 2, pp. 127-136.

W. Xiong, B. Wietbrock, A. Saeed-Akbari, M. Bambach, G. Hirt: Steel research international, 82 (2011) No. 1, pp. 63-69

* ρ and C_p from TCFE4

Material characterization – results of compression tests at RT



- Mn28C0.3 / 0,1 1/s
- △— Mn28C0.3 / 1 1/s
- Mn28C0.3 / 10 1/s
- Mn22C0.6 / 0,1 1/s
- △— Mn22C0.6 / 1 1/s
- Mn22C0.6 / 10 1/s
- Mn22C0.3 / 0,1 1/s
- △— Mn22C0.3 / 1 1/s
- Mn22C0.3 / 10 1/s
- AISI304/ X5CrNi18-10 / 0,1 1/s
- △— AISI304/ X5CrNi18-10 / 1 1/s
- AISI304/ X5CrNi18-10 / 10 1/s

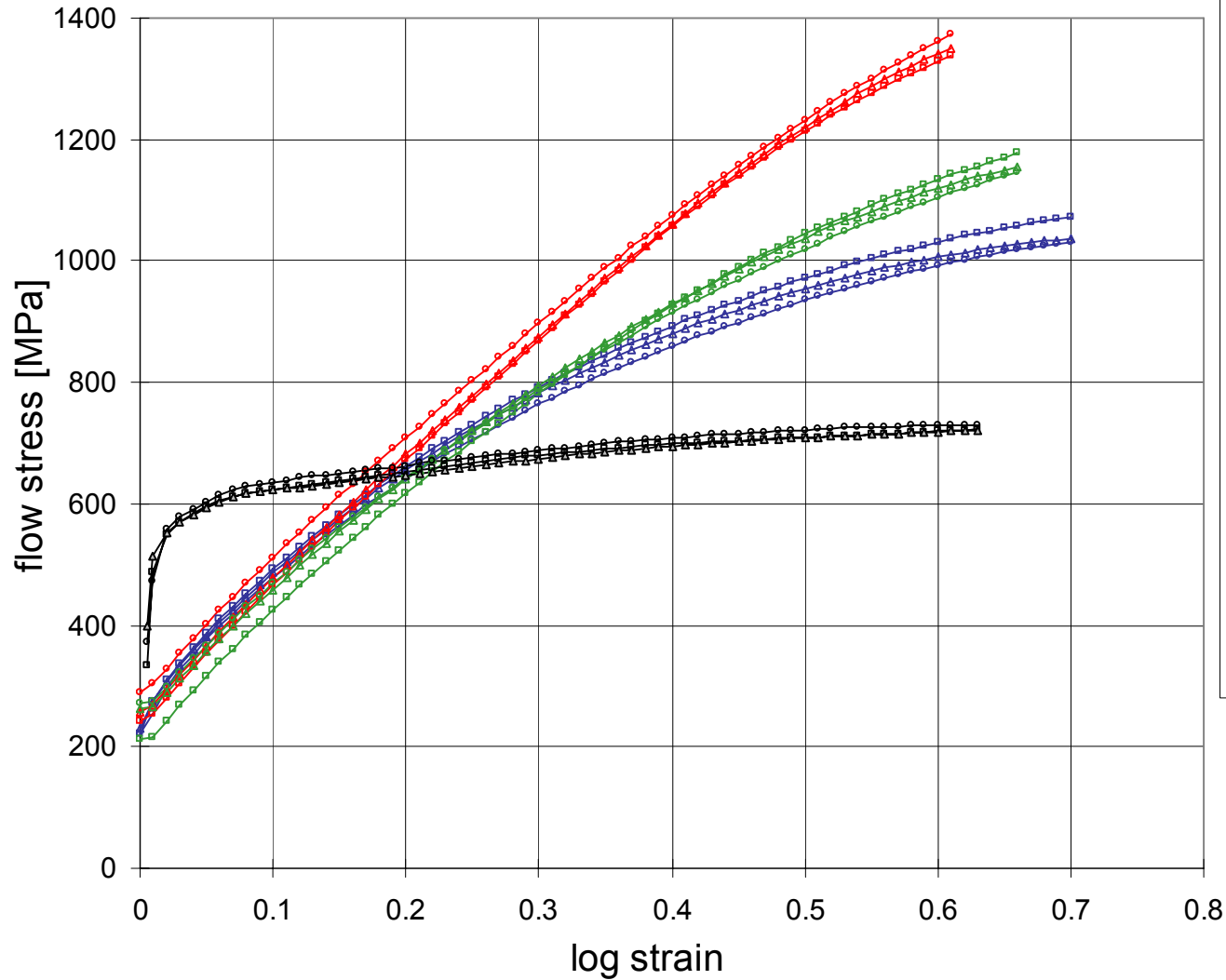
Carbon content leads to different strain hardening behaviour

Increasing manganese content reduces maximum strength

With increasing strain rate flow stress slope is reduced

Reference material: AISI 304, (1.4301, X5CrNi18-10), isothermal compression tests on cold drawn steel material

Material characterization – results of compression tests at 300°C

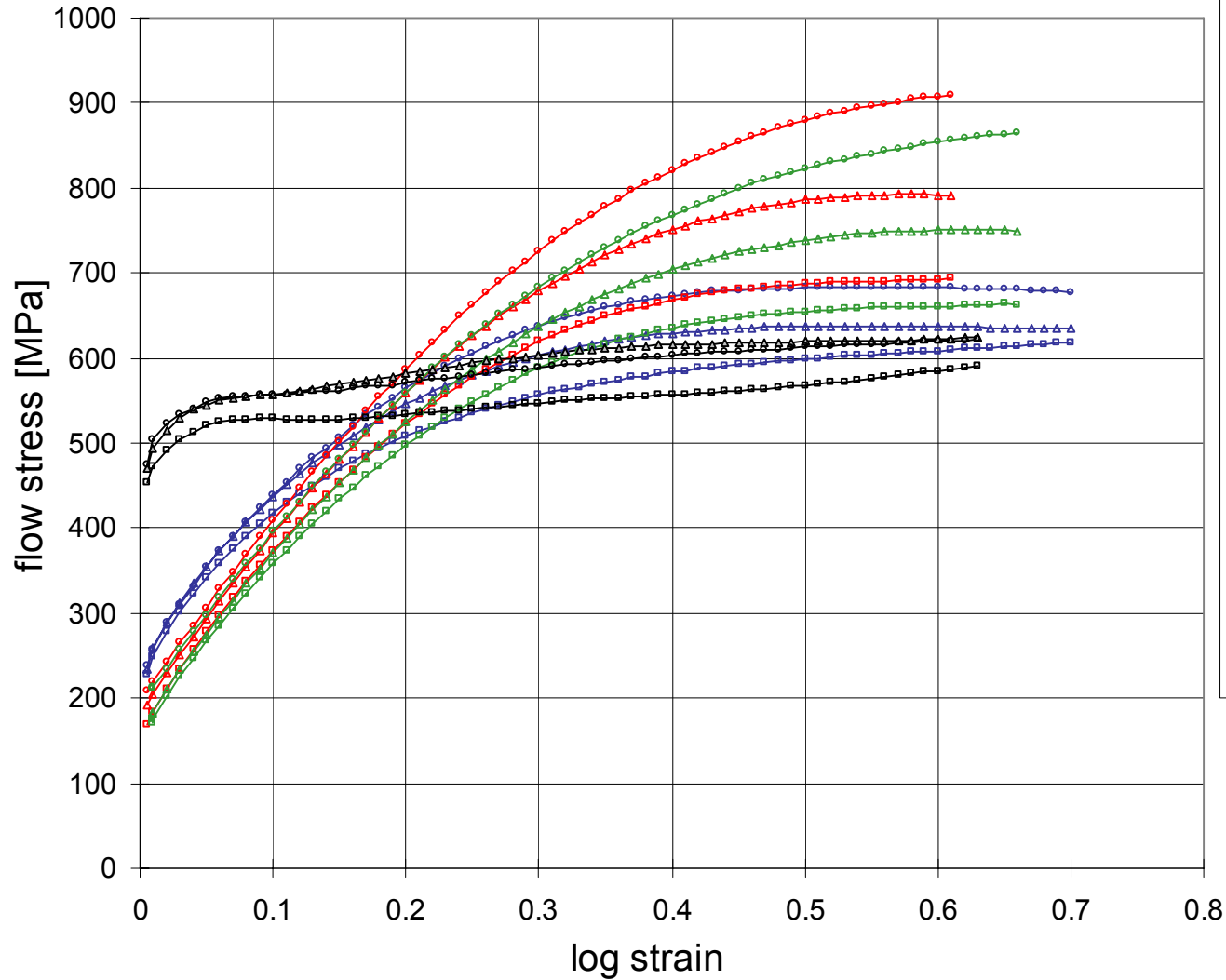


- Mn28C0.3 / 0,1 1/s
- △— Mn28C0.3 / 1 1/s
- Mn28C0.3 / 10 1/s
- Mn22C0.6 / 0,1 1/s
- △— Mn22C0.6 / 1 1/s
- Mn22C0.6 / 10 1/s
- Mn22C0.3 / 0,1 1/s
- △— Mn22C0.3 / 1 1/s
- Mn22C0.3 / 10 1/s
- AISI304/ X5CrNi18-10 / 0,1 1/s
- △— AISI304/ X5CrNi18-10 / 1 1/s
- AISI304/ X5CrNi18-10 / 10 1/s

Increasing carbon content leads to higher maximum strength
 Increasing manganese content reduces maximum strength
 No influence of strain rate
 Maximum flow stress 2 times of AISI304

Reference material: AISI 304, (1.4301, X5CrNi18-10), isothermal compression tests on cold drawn steel material

Material characterization – results of compression tests at 500°C



- Mn28C0.3 / 0,1 1/s
- △— Mn28C0.3 / 1 1/s
- Mn28C0.3 / 10 1/s
- Mn22C0.6 / 0,1 1/s
- △— Mn22C0.6 / 1 1/s
- Mn22C0.6 / 10 1/s
- Mn22C0.3 / 0,1 1/s
- △— Mn22C0.3 / 1 1/s
- Mn22C0.3 / 10 1/s
- AISI304/ X5CrNi18-10 / 0,1 1/s
- △— AISI304/ X5CrNi18-10 / 1 1/s
- AISI304/ X5CrNi18-10 / 10 1/s

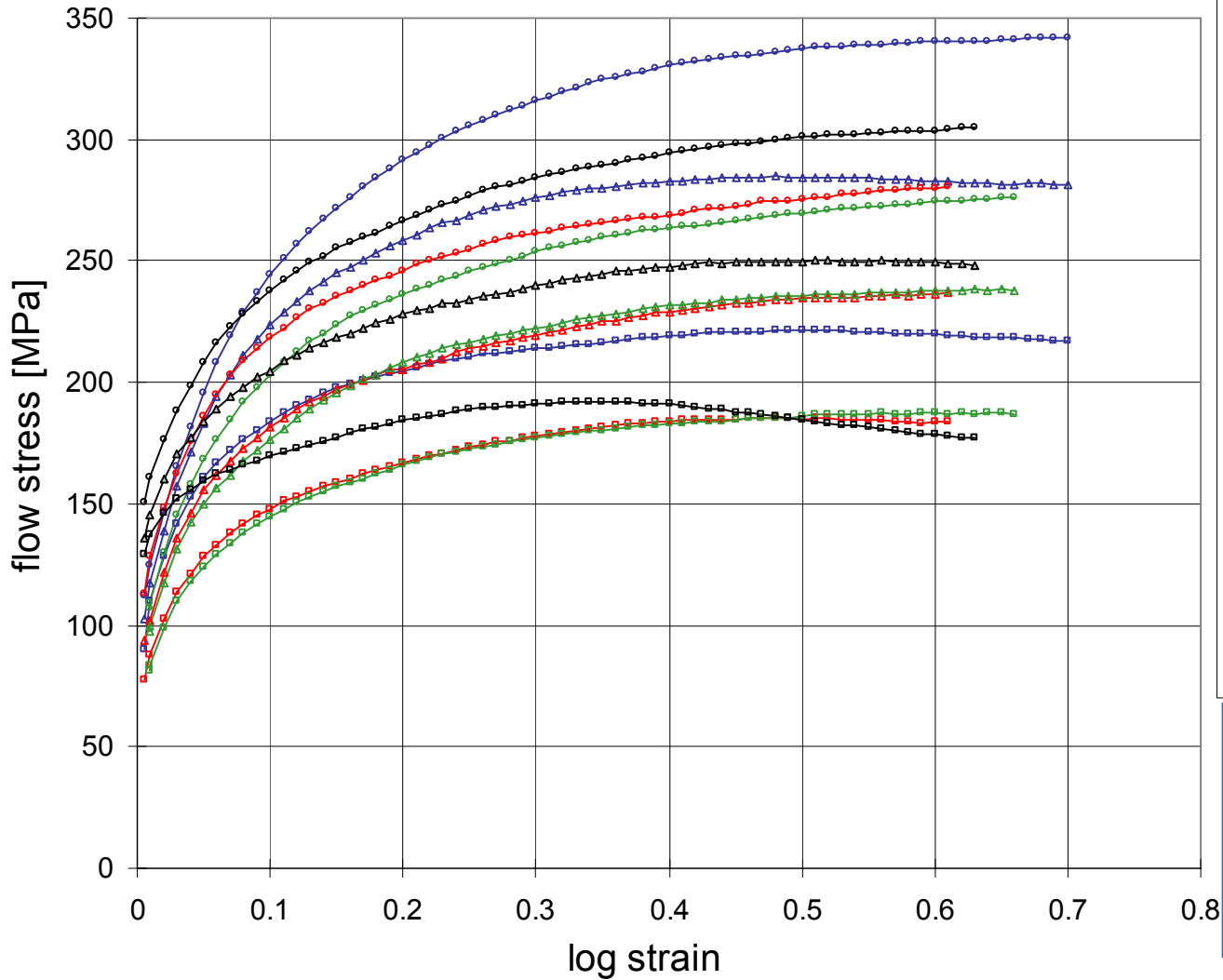
Increasing carbon content leads to higher maximum strength

Increasing manganese content reduces maximum strength

With increasing strain rate flow stress slope is increased

Reference material: AISI 304, (1.4301, X5CrNi18-10), isothermal compression tests on cold drawn steel material

Material characterization – results of compression tests at 900°C



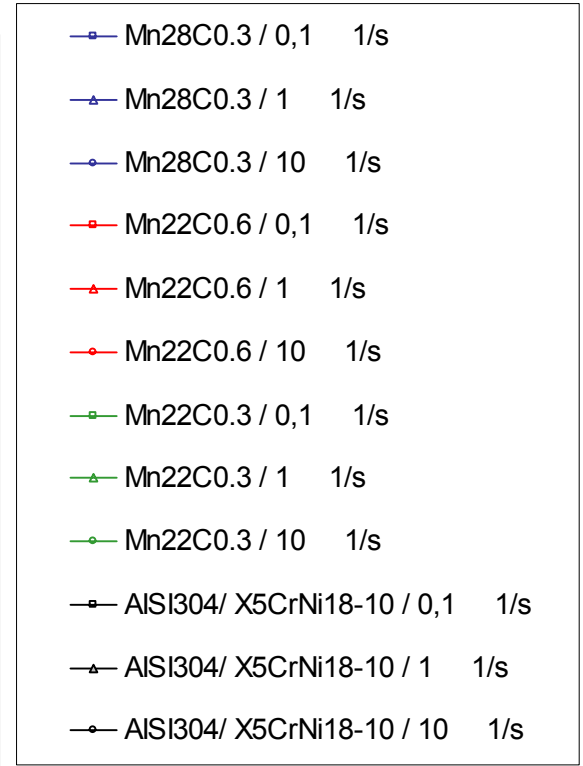
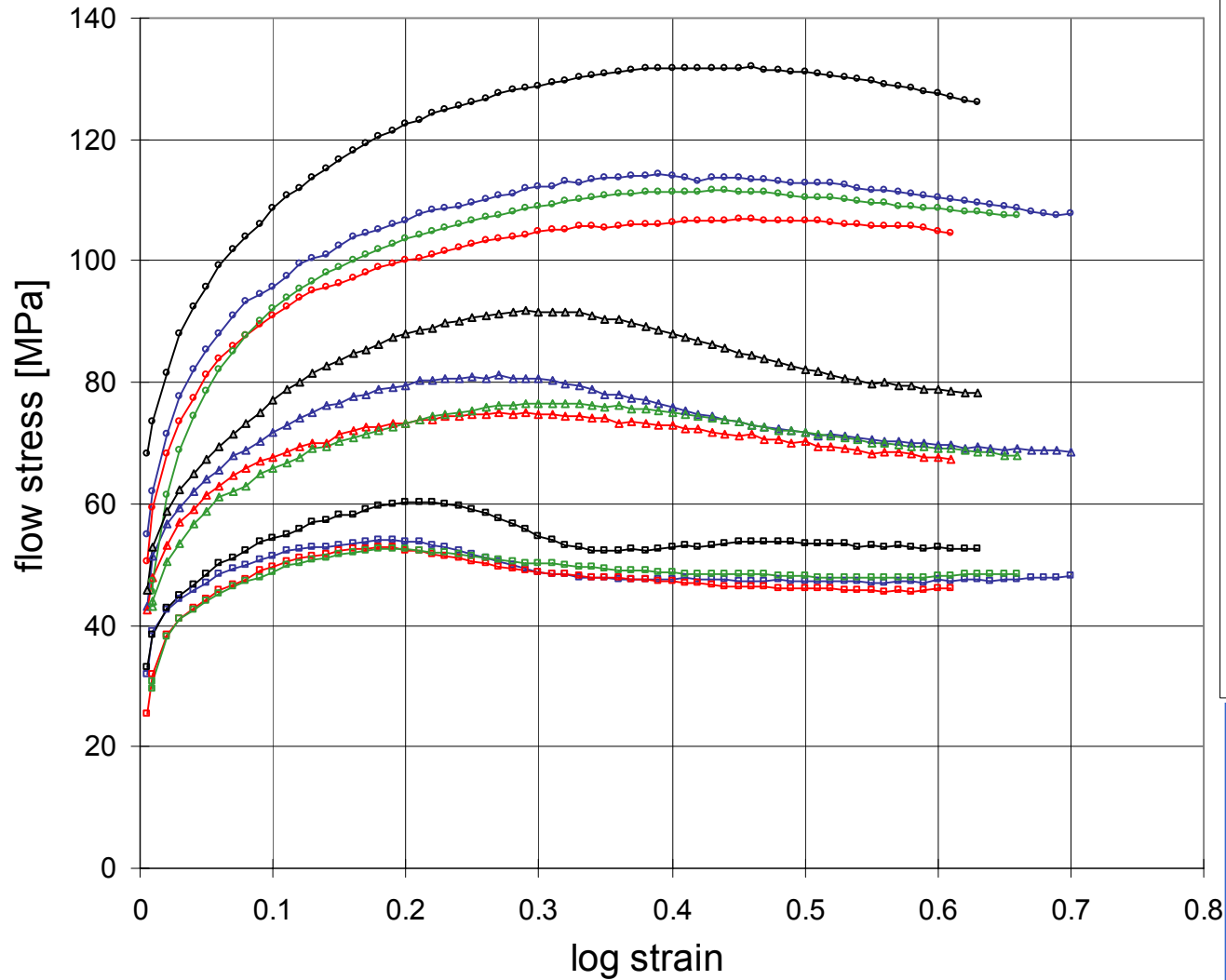
- Mn28C0.3 / 0,1 1/s
- △— Mn28C0.3 / 1 1/s
- Mn28C0.3 / 10 1/s
- Mn22C0.6 / 0,1 1/s
- △— Mn22C0.6 / 1 1/s
- Mn22C0.6 / 10 1/s
- Mn22C0.3 / 0,1 1/s
- △— Mn22C0.3 / 1 1/s
- Mn22C0.3 / 10 1/s
- AISI304/ X5CrNi18-10 / 0,1 1/s
- △— AISI304/ X5CrNi18-10 / 1 1/s
- AISI304/ X5CrNi18-10 / 10 1/s

Carbon content shows small influence,
 increasing manganese content
 increases flow stresses

Flow stresses of AISI are in the same
 order as those of HMS

Reference material: AISI 304, (1.4301, X5CrNi18-10), isothermal compression tests on cold drawn steel material

Material characterization – results of compression tests at 1200°C



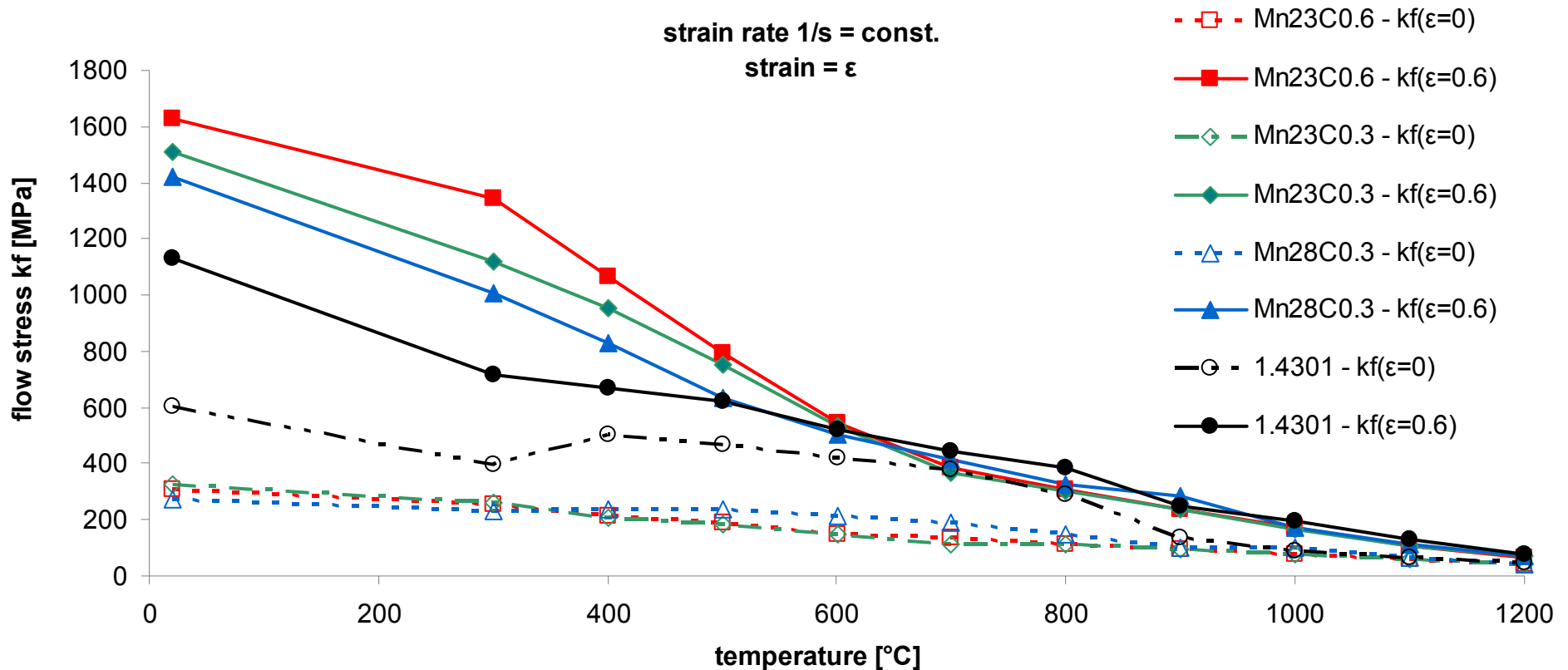
Carbon and manganese content show small influence

Flow stresses of AISI are higher than those of HMS

Flow stress of HMS 4 to 6 times smaller than at 700°C

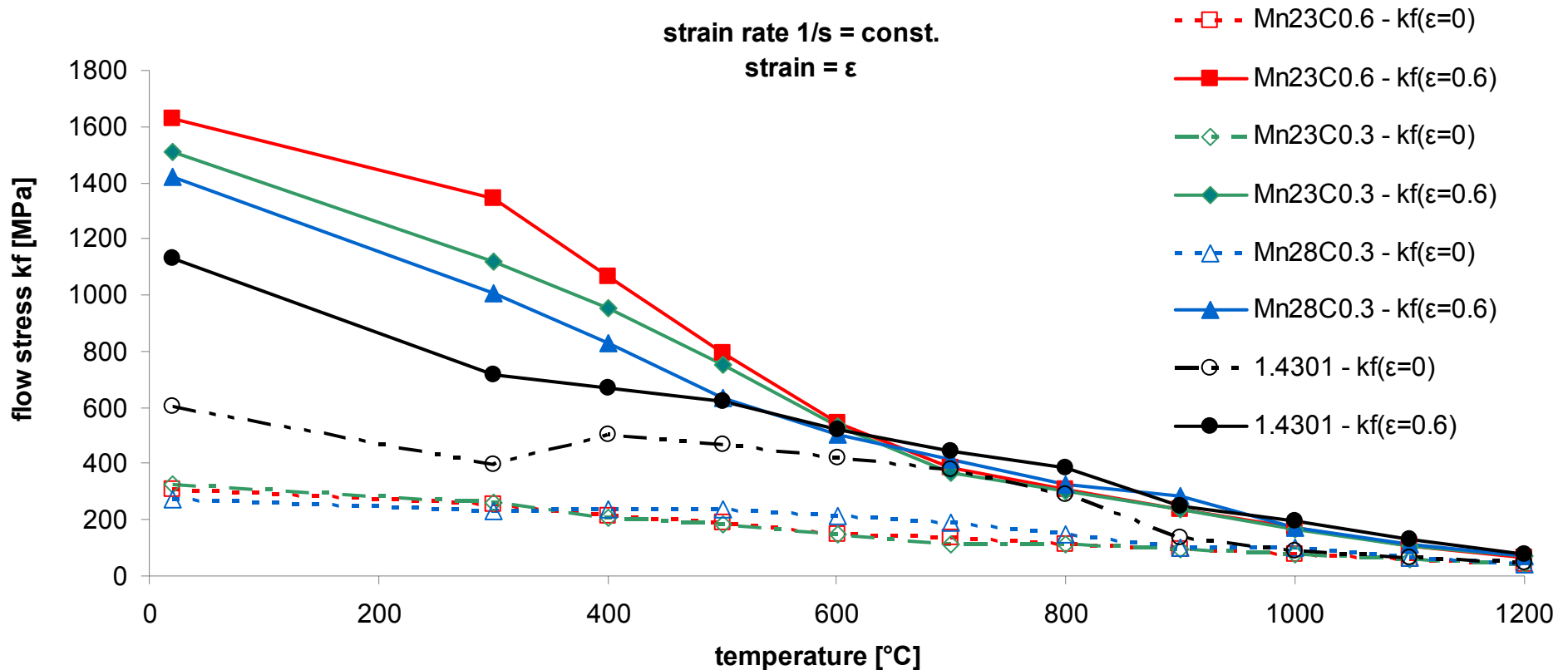
Reference material: AISI 304, (1.4301, X5CrNi18-10), isothermal compression tests on cold drawn steel material

Material characterization – summary of compression tests I



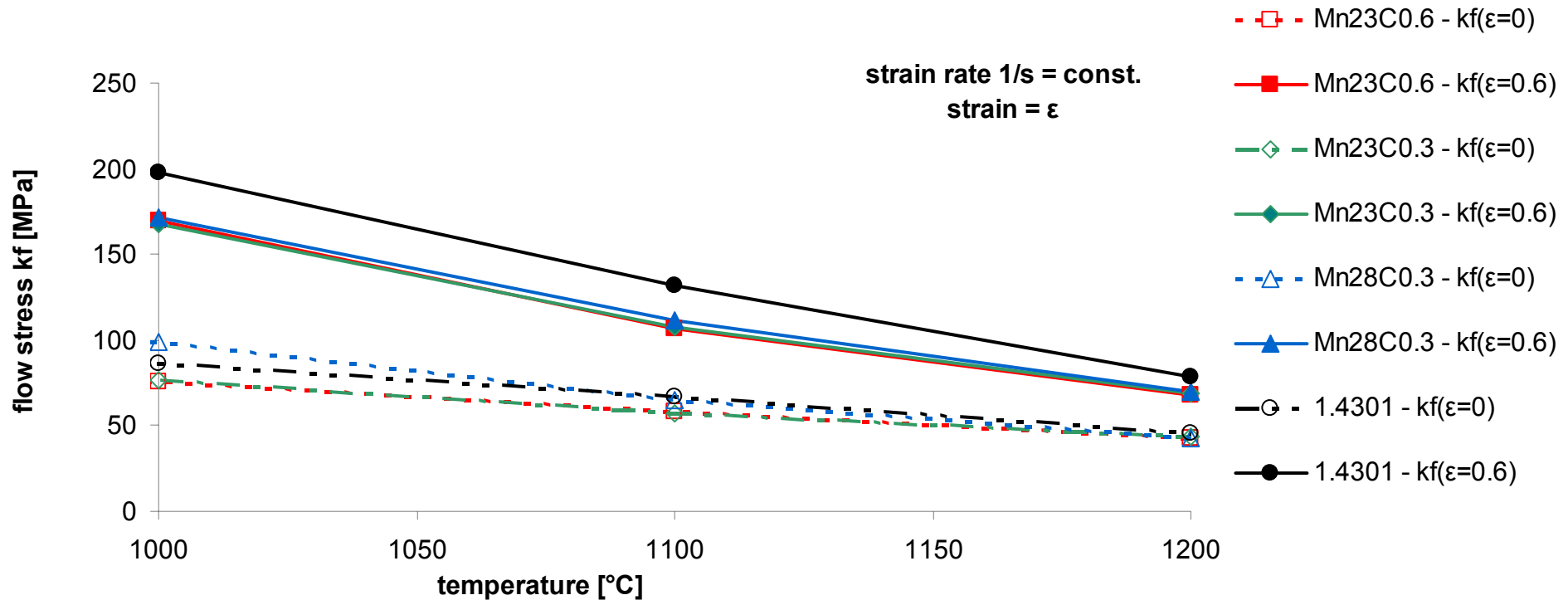
At smaller temperatures (RT to 600°C):

- Higher carbon content (0.6 to 0.3 wt.%) leads to higher stresses
- Higher manganese (28 to 22 wt.%) content reduces maximum flow stresses
- Incipient yielding of all HMnS is lower than of 1.4301 / AISI 304 while strengthening is higher



At middle temperatures (700 to 900°C):

- Maximum flow stresses are comparable to steel 1.4301 / AISI 304
- Higher manganese content increases maximum flow stresses and incipient yielding
- Influence of carbon content becomes smaller, but increases the maximum flow stress



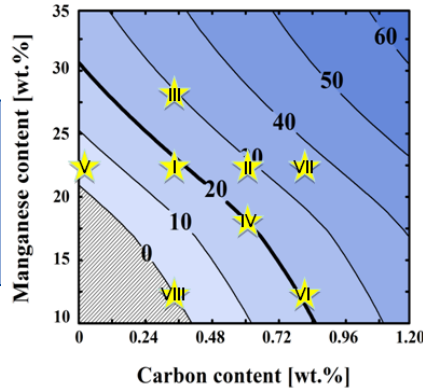
At higher temperatures (1000 to 1200°C):

- Carbon content has negligible influence on flow curves
- Higher manganese content has small but increasing influence on flow stresses
- Flow stresses are lower than those of steel 1.4301 / AISI 304



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Process Chain of Material Production



Vacuum melting (IEHK)



Forging and annealing (IBF)



Hot and cold rolling (IBF)

Design of 8 different Fe-Mn-C compositions based on SFE (IEHK)¹

Casting: 140*140 mm² cross section and up to 100 kg weight

FG: 3 passes (1150°C) to 55 mm height, AN: 1150°C 5 hours

HR: 12 passes (1150°C) to <3 mm height
CR: up to 80% reduction

Problems encountered

- **Inhomogeneities** of the Mn (8%) and C (0.3%) content in the micro scale (cast state)

Solution: Process chain developed, reducing segregations to Mn: 2% and C: 0.05%²

- **Strong oxidation** during heating and annealing caused enrolled scale

Solution in the laboratory process chain: high pressure water jet

- Small possible **cold reduction rates** of only 15-20 % of TRIP compositions

1) Saeed-Akbari, A.; Imlau, J.; Prah, U. and Bleck, W., Derivation and Variation in Composition-Dependent Stacking Fault Energy Maps Based on Subregular Solution Model in High-Manganese Steels, Metallurgical Materials Transactions A, Vol. 40A, Dec. 2009, pp. 3076-3090
2) Wietbrock, B.; Bambach, M.; Seuren, S.; Hirt, G., Homogenization strategy and material characterization of high-manganese TRIP and TWIP steels, Materials Science Forum (2010) Vols. 638-642, pp. 3134-3139



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Thank You for Your attention

